

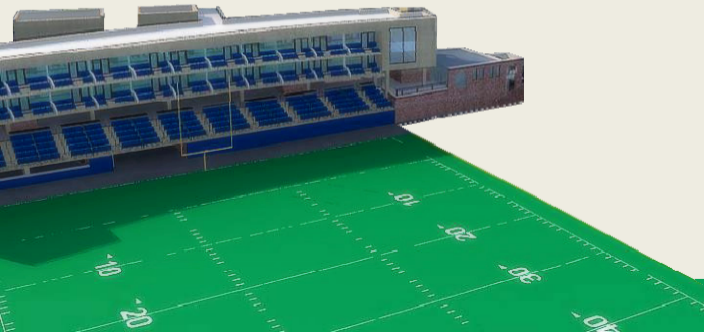
# GAME DAY BUILDING POST TENSIONED REDESIGN

AE SENIOR THESIS SPRING 2009

MATTHEW HAAPALA

BAE/MAE STRUCTURAL OPTION

FACULTY CONSULTANT: DR. HANAGAN



## PRESENTATION OUTLINE

- Existing Conditions
- Thesis Proposals and Goals
- Gravity System Redesign
- Lateral System Redesign
- Foundation Optimization
- Cost & Schedule Analysis
- Lighting Redesign
- Conclusions
- Question and Answer

# GAME DAY BUILDING POST TENSIONED REDESIGN

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•EXISTING CONDITIONS

•THESIS PROPOSAL & GOALS

•GRAVITY SYSTEM REDESIGN

•LATERAL SYSTEM REDESIGN

•FOUNDATION OPTIMIZATION

•COST & SCHEDULE ANALYSIS

•LIGHTING REDESIGN

•CONCLUSIONS

## BUILDING STATISTICS

Building Name: Foreman Field Game Day Building

Project Team:

- Owner - Old Dominion University
- General Contractor - S.B. Ballard Construction Company
- Architect - Ellerbe Becket
- Engineer - Clark Nexsen

Size : Gross Floor Area = 54,877 sq. ft. , Height = 47 ft.

- 1<sup>st</sup> Floor = 16,500 sq. ft.
- 2<sup>nd</sup> Floor = 16,100 sq. ft.
- 3<sup>rd</sup> Floor = 11,500 sq. ft.
- 4<sup>th</sup> Floor = 10,800 sq. ft.

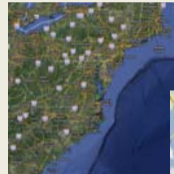
Construction: Dates of February 22, 2008 thru July 22, 2009

Cost: \$11.9 million

Project Delivery Method: Design-Building

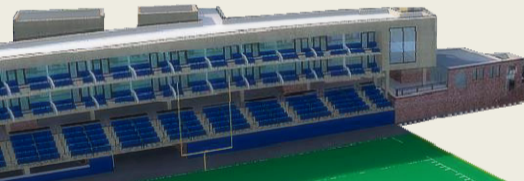
## BUILDING STATISTICS

Location: The Game Day building is currently under construction in the south end zone of Foreman Field on the campus of Old Dominion University in Norfolk Virginia.



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## EXISTING GRAVITY SYSTEM

### Cast in Place Reinforced Concrete Flat Plate

- Typical bay size 31'-6" x 17'-0"
- Typical slab depth 12"
- No shear caps or drop panels
- Shear stud rails used to resist punching shear

### Cast in Place Reinforced Concrete Beams

- Located around openings and seating

### Cast in Place Concrete Columns

- 18" x 18" typical

## 3<sup>RD</sup> FLOOR STRUCTURAL PLAN



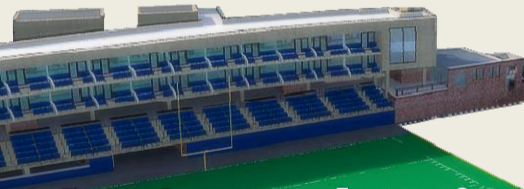
Blue: Beam Location

Red: Column or Load Bearing Wall Location

# GAME DAY BUILDING

## POST TENSIONED REDESIGN

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## EXISTING LATERAL SYSTEM

- Seven Cast in Place Reinforced Concrete Shear Walls
- Located in Architecturally Convenient Locations

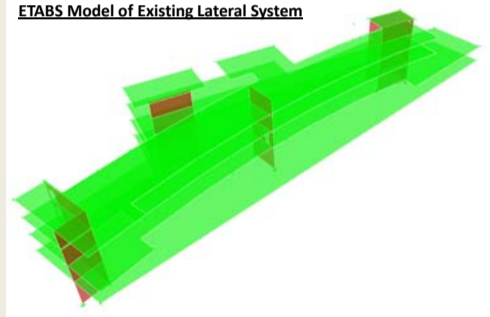
Shear Wall Location Plan



## EXISTING LATERAL SYSTEM

- Capacity Significantly Exceeds Lateral Loading Demands
- Column & Slab Moment Frames' Stiffness not Considered

ETABS Model of Existing Lateral System



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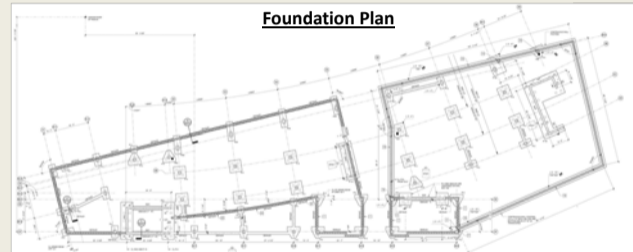
•CONCLUSIONS

## EXISTING FOUNDATIONS

- Square Precast Prestressed Concrete (SPPC) Piles
- 100' long from Tip to Cutoff
- 183 Piles Total
- Typically Driven in Clusters of 4 Below Most Columns
- Clusters of Up to 18 Below Shear Walls
- Topped With 36" - 40" Deep Pile Caps
- Grade Beams Below Exterior Walls & Between Pile Caps

Sub-Surface Soil Conditions	
Average Depth (ft.)	Description
0 to 1	Topsoil or Asphalt
0 to 4	Fill of fibrous organics and wet sand
2 to 18	Sand with varying amounts of silt and clay
18 to 53-84	Gray, wet clay with varying amounts of sand and marine shell fragments
53-84 to 110	Gray, wet, silty, fine sand with marine shell fragments and varying amounts of clay

## EXISTING FOUNDATIONS



# GAME DAY BUILDING

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## STRUCTURAL DEPTH PROPOSAL

### Study 1 Gravity System Redesign

Problem: Two-way flat plate is structurally inefficient floor system

Solution: Replace with one-way slabs on post tensioned beams

Goals:

- Reduce slab depth
- Develop understanding of post tensioned concrete design
- Use post tensioning to minimize beam depth
- Reduce self weight of the structure

## STRUCTURAL DEPTH PROPOSAL

### Study 2 Lateral System Redesign

Problem: Shear walls' excess capacity suggests reduction possible

Solution: Consider Moment Frames in Lateral Design and Remove Existing Shear Walls Where Practical

Goals:

- Utilize Post Tensioned Beams in Ordinary Concrete Moment Frames
- Reduce The Number of Shear Walls

### Study 3 Foundation Optimization

Problem: With poor soils extensive deep foundations required

Solution: Analyze foundation requirements of redesigned structure to determine possible foundation reductions

Goal: Reduce the number of piles

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## C.M. BREADTH PROPOSALS

Problem: Unknown cost, constructability, and construction schedule impacts of structural redesign

Solution: Conduct cost and schedule analyses comparing of the original and redesigned structure

Goals:

- Lower the price of the structure
- Develop a construction sequence that satisfies the unique demands of post tensioning
- Do not Increase the Overall Project Duration

## C.M. BREADTH PROPOSALS





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## LIGHTING BREADTH PROPOSAL

Problem: Original lighting design predominantly inexpensive troffers and cans

Solution: Create an alternate lighting scheme for the scholarship lounge

Goals:

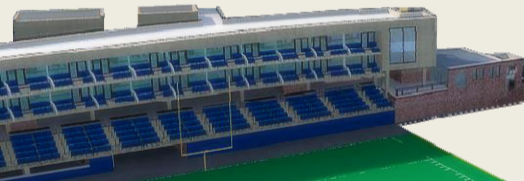
- Integrate the structural redesign into the redesigned lighting scheme
- Make the room seem more spacious have emphasizing the peripherals by having a high luminance on the Walls and Ceiling.
- Increase flexibility by specifying dimmable fixtures
- Satisfy ASHRE 90.1 and IESNA Lighting Handbook requirements
- Use attractive or concealed luminaries

## LIGHTING BREADTH PROPOSAL



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## GRAVITY SYSTEM REDESIGN

### Reference Design Codes and Standards

Original Design Code	Substitutions
2003 Virginia Uniform Statewide Building Code	2006 IBC
ASCE 7-02	ASCE 7-05
ACI 318-02	ACI 318 08



Concrete Material Properties	Original		New	
	f'c (psi)	Cement Type	f'c (psi)	Cement Type
Pile Caps and Grade Beams	3000	I	3000	I
Slabs on Grade	3000	I	3000	I
Structural Slabs and Beams	5000	I	6000	III
Walls and Columns	5000	I	6000	III

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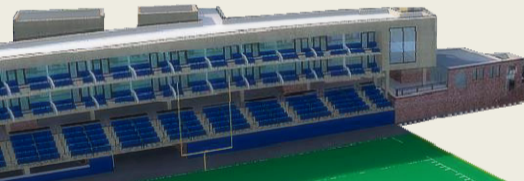
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## GRAVITY LOADING ASSUMPTIONS

GRAVITY LOADING DESIGN VALUES		
Loading	Design Value	ASCE 7-05 Req'd
<b>Dead Loads</b>		
Normal Weight Concrete	150 pcf	
Masonry Walls	40 psf	
Curtin Walls	15 psf	
Mechanical/Electrical/Plumbing	5 psf	
100% Outdoor Air Handling Unit	750 lbs	
Variable Refrigerant Volume Heat Pump	350 lbs	
Gas Fired DX Package Roof top Unit	500 lbs	
DX Split System Heat Pump	250 lbs	
<b>Live Loads</b>		
ROOF	20 psf	20 psf
STAIRS	100 psf	100 psf
CORRIDORS	100 psf	100 psf
TERRACES	100 psf	100 psf
SEATING	100 psf	60 psf
STORAGE	125 psf	125 psf
MECH./ELEC. ROOMS	125 psf	
<b>Snow Loads</b>		
Pg	10 psf	10 psf
Pf	11 psf	11 psf

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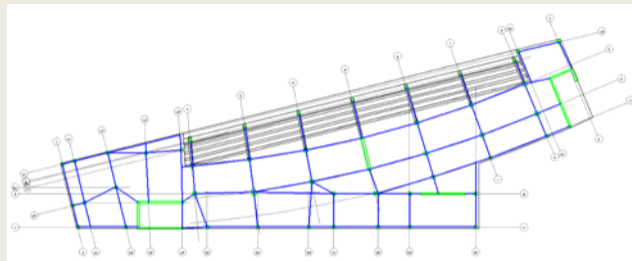
•FOUNDATION OPTIMIZATION




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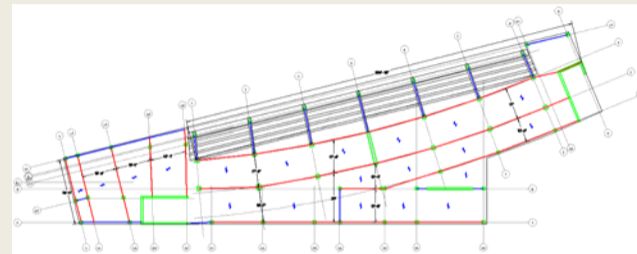
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## TRIAL LAYOUT DEVELOPMENT



-  = Post Tensioned Concrete Beam
-  = Reinforced Concrete Beam
-  = Support Column or Wall

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-  = Post Tensioned Concrete Beam
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# GAME DAY BUILDING

## POST TENSIONED REDESIGN

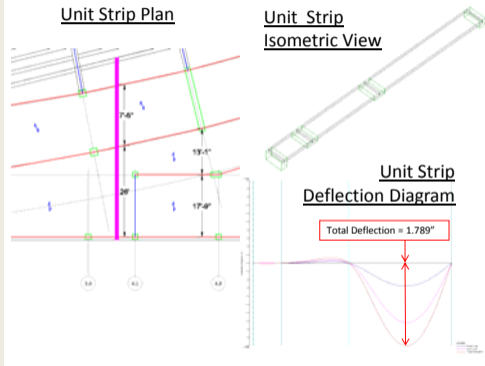
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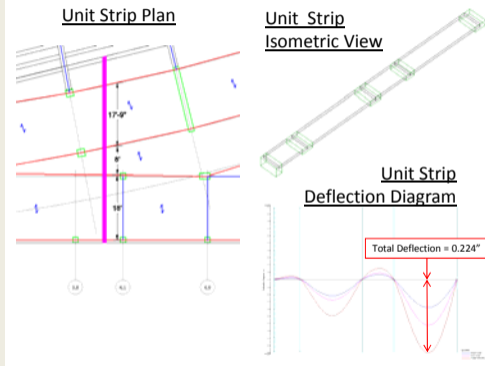
## PCA SLAB ANALYSIS & DESIGN

PCA Slab Unit Strip 2<sup>nd</sup> Floor Between Gridlines 3.8 and 4.1 w/ Initial Beam Layout



## PCA SLAB ANALYSIS & DESIGN

PCA Slab Unit Strip 2<sup>nd</sup> Floor Between Gridlines 3.8 and 4.1 w/ Final Beam Layout



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## PT BEAM HAND CALCULATIONS

### Calculations

- Designed in accordance with ACI 318-08 for:
  - Flexural serviceability
  - Ultimate flexural strength
  - Shear and torsion
  - Deflection
- Every post tensioned beam analyzed at supports and midspan
- Member loads determined by iterative moment distribution
  - Pattern loading not critical
  - Moment redistribution not performed
    - $\epsilon_t > .0075$  (ACI 318-08 Sect. 8.4.2)
- Beam/Slab effective T beams considered

# GAME DAY BUILDING

## POST TENSIONED REDESIGN

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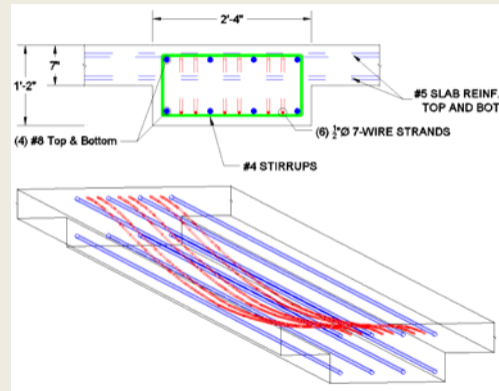
•LATERAL SYSTEM REDESIGN

•CONCLUSIONS

## PT BEAM HAND CALCULATIONS

- Interior beams
  - Depth: 14" = 2x slab depth of 7"
  - Width: 12" - 40", typ. 28"
  - # Tendons: (5) - (13), typ. (6)
  - Longitudinal Rebar: (3) - (5) #8 Top & Bottom , typ. (4)
- Perimeter beams: depth 18"
  - Depth 18" - 29"
  - Width 12" - 24", typ. 18"
  - # Tendons: (4) - (6), typ. (4)
  - Longitudinal Rebar : (2) - (4) #8 Top & Bottom, typ. (2)
- On average 76% dead load balanced after losses
- Average Compressive Stress 164psi – 475psi, typ. 250 psi
  - > Code required 125psi
  - < 500psi reasonable maximum

## PT BEAM HAND CALCULATIONS



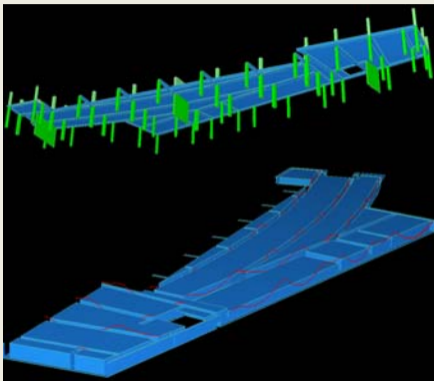
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## RAM CONCEPT ANALYSIS





# GAME DAY BUILDING

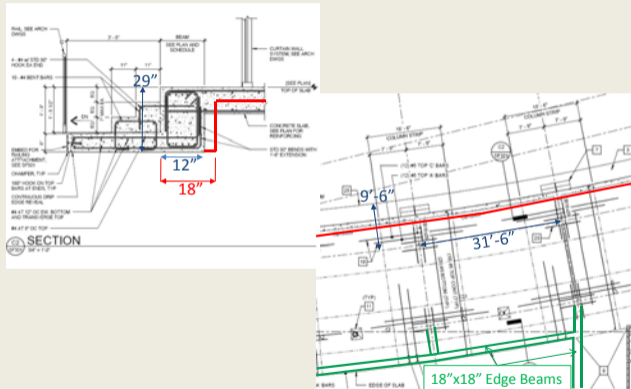
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## TORSION & DEFLECTION DESIGN



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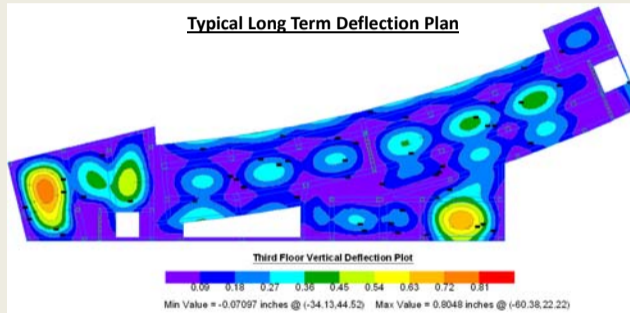
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## TORSION & DEFLECTION DESIGN

Typical Long Term Deflection Plan



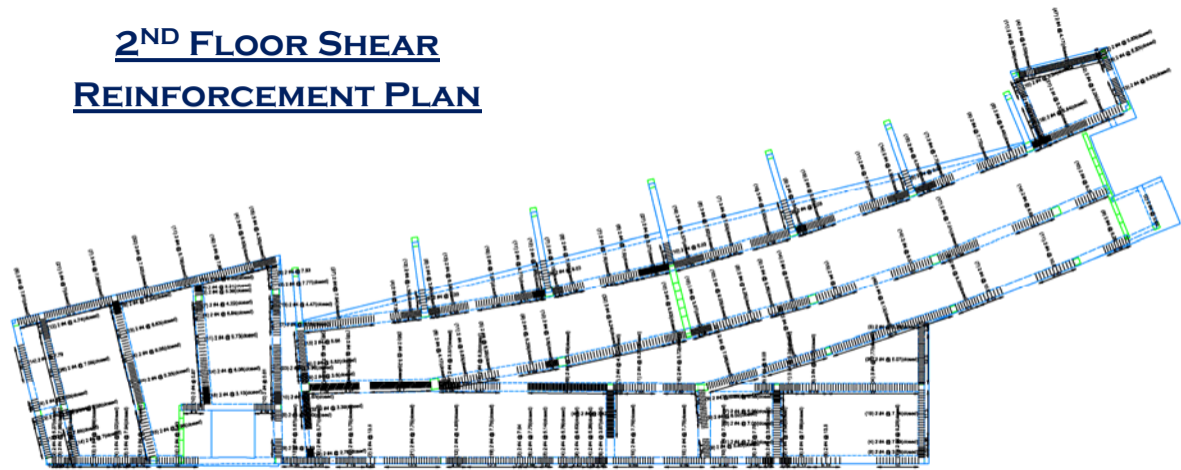
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## 2<sup>ND</sup> FLOOR SHEAR REINFORCEMENT PLAN





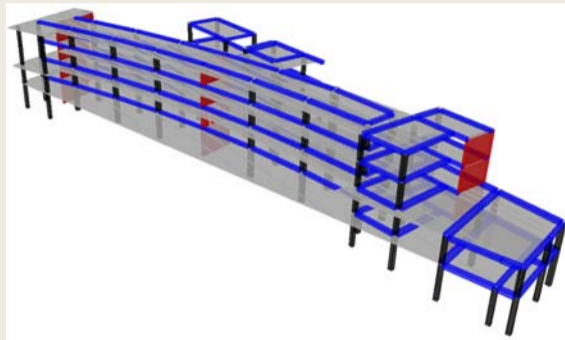
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## LATERAL SYSTEM REDESIGN



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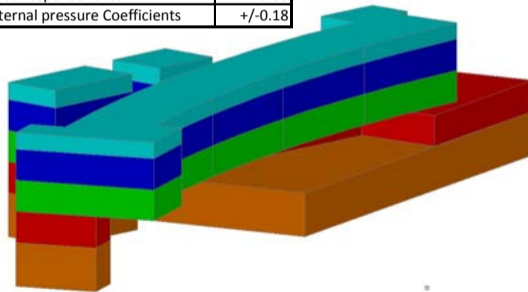
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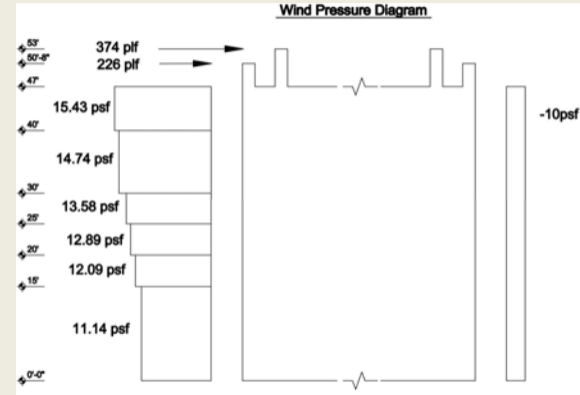
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## WIND LOADING

Wind Loading Design Values	
Basic Wind Speed	110MPH
Wind Importance Factor	1.15
Wind Exposure Category	B
Gust Response Factor	0.85
Internal pressure Coefficients	+/-0.18



## WIND LOADING



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## SEISMIC LOADING

Seismic Design Values	
Site Class	D
Importance Factor, I	1.25
$S_s$	0.118
$S_1$	0.048
$F_a$	1.6
$F_v$	2.4
$S_{DS} = (2/3) * F_a * S_s$	0.126
$S_{D1} = (2/3) * F_v * S_1$	0.0768
Seismic Design Category	B
Building Height, h	47'
$C_t$	0.02
x	0.75
$T_a = C_t * h^x$	0.359
$C_u$	1.7
$C_u T_a$	0.61
$T_L$	8

## SEISMIC LOADING

Design Coefficients for Seismic Force Resisting Systems		
Seismic Force Resisting System	Response Modification Coefficient, R	Deflection Amplification Factor, $C_d$
Ordinary Reinforced Concrete Moment Frames	3	2.5
Ordinary Reinforced Concrete Shear Walls	5	4.5
Ordinary Reinforced Concrete Moment Frames and Ordinary Reinforced Concrete Shear Walls	4.5	4

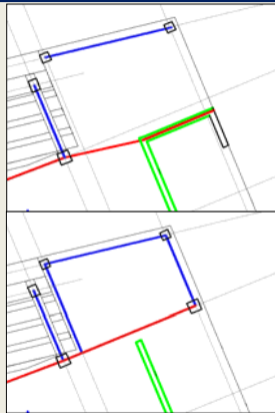
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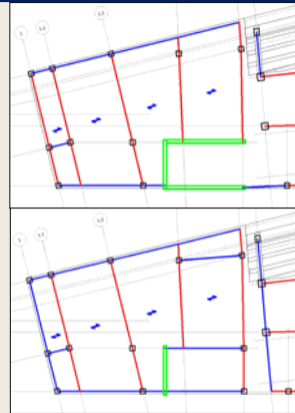


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## SHEAR WALL 7 REMOVAL



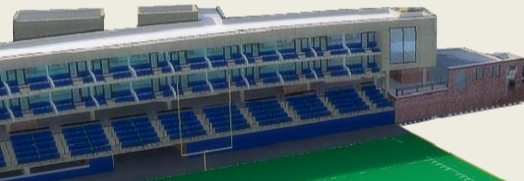
## SHEAR WALLS 1 & 3 REMOVAL





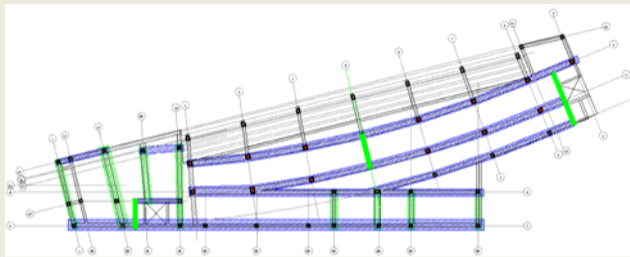
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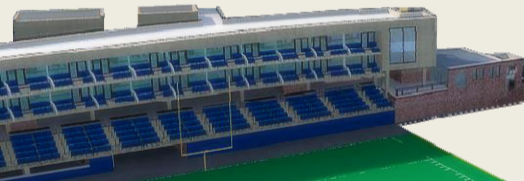
## LATERAL SYSTEM PLAN



-  = Columns Sections Increased
-  = Plan East/West Direction Lateral System Components
-  = Plan North/South Direction Lateral System Components

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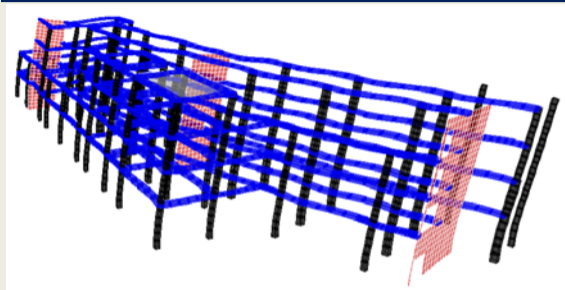
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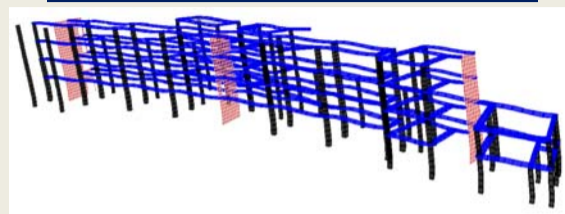
•CONCLUSIONS

## SOUTH WIND DEFLECTED SHAPE



Max Deflections Caused By Wind Loading				
Story	Max Deflection X (in.)	Max Deflection Y (in.)	h/600 (in.)	Deflection Check (OK or NG)
Roof	0.0686	0.0868	0.2133	OK
Floor 4	0.0709	0.0401	0.2133	OK
Floor 3	0.0707	0.0376	0.2133	OK
Floor 2	0.0684	0.0340	0.3000	OK

## SEISMIC DEFLECTED SHAPE



Seismic Drift Analysis						
East/West Direction						
Story	Cd	Average Diaphragm Drift	Max Diaphragm Drift	Seismic Drift Limit	Drift Limit Exceeded	Torsional Irregularity
Roof	2.5	0.002915	0.002953	0.02	No	No
Floor 4	2.5	0.003378	0.003418	0.02	No	No
Floor 3	2.5	0.003383	0.003418	0.02	No	No
Floor 2	2.5	0.002220	0.002245	0.02	No	No
North South Direction						
Story	Cd	Average Diaphragm Drift (Y)	Max Diaphragm Drift (Y)	Seismic Drift Limit	Drift Limit Exceeded	Torsional Irregularity
Roof	4	0.001120	0.001204	0.02	No	No
Floor 4	4	0.000816	0.000960	0.02	No	No
Floor 3	4	0.000816	0.000884	0.02	No	No
Floor 2	4	0.000396	0.000472	0.02	No	No

# GAME DAY BUILDING

## POST TENSIONED REDESIGN

BY: MATTHEW HAAPALA



• EXISTING CONDITIONS

• FOUNDATION OPTIMIZATION

• THESIS PROPOSAL & GOALS

• COST & SCHEDULE ANALYSIS

• GRAVITY SYSTEM REDESIGN

• LIGHTING REDESIGN

• LATERAL SYSTEM REDESIGN

• CONCLUSIONS

## SHEAR WALL DESIGN

Load Combo	Loading			
	1.2D+1.6W+L	0.9D+1.6W	1.2D+1.0E+L	0.9D+1.0E
$P_u$ (Kips)	1127	606	1128	606
$V_u$ (Kips)	174	201	27	54
$M_u$ (K-ft)	8001	7965	3370	3333

Design Values	
$\phi$ Tension	0.9
$\phi$ Shear	0.75
$\phi$ Comp.	0.65

Geometry	
$h_w$ (in)	222
$h$ (in)	18
$h_w$ (in)	180
$d$ %	80.00%
$A$ (in <sup>2</sup> )	3996
$S$ (in <sup>3</sup> )	147852
$I$ (in <sup>4</sup> )	16411572

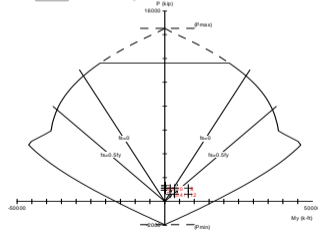
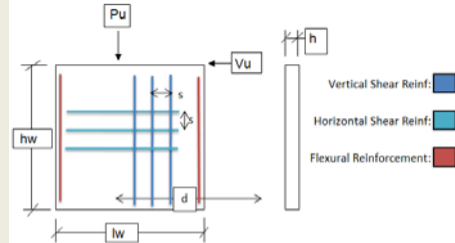
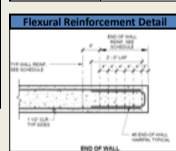
Material Properties	
$f'_c$	6000
$f_y$	60000

Shear Reinforcement Req'd	
# of Curtains Req'd	1
$A_s$ min (in <sup>2</sup> /ft)	0.54
Max Spacing (in)	13.78

Shear Reinforcement Design	
# of Curtains	2
Bar Size	#5
Bar Spacing (in)	12
$\rho_c$	3
$\rho_t$	0.006
$\phi V_n$ (Kips)	268
$V_u / \phi V_n$	75%

Flexural Reinforcement Req'd	
Boundary Zone	No

Flexural Reinforcement Design	
# of Bars	7
Bar Size	#9
$\phi M_n > M_u, \phi P_n > P_u$	Yes



# GAME DAY BUILDING POST TENSIONED REDESIGN

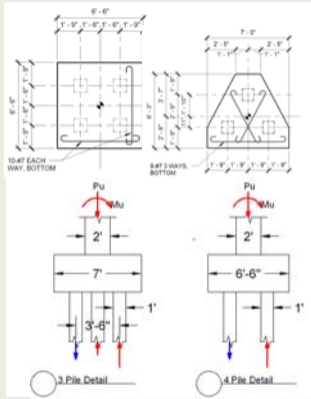
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## FOUNDATION OPTIMIZATION



Location	LIVE Load (K/ft)	DEAD Load (K/ft)	P-Force (K)	M (K-ft)	# of Piles	
					Original	Final
1.1.1	21.94	8.01	99	90.1	2	2
1.1.2	23.34	-0.71	99	90.1	2	2
1.2.1	25.74	2.01	99	90.1	2	2
1.2.2	25.95	8.22	99	90.1	2	2
1.3	22.41	4.39	99	90.1	2	2
1.3.1	23.81	-7.91	99	90.1	2	2
1.3.2	49.22	23.94	99	90.1	2	2
1.4	27.44	-12.74	99	90.1	2	2
1.4.1	22.42	25.39	99	90.1	2	2
1.4.2	48.75	11.72	99	90.1	2	2
1.5	32.48	18.37	99	90.1	2	2
1.6	25.07	6.11	99	90.1	2	2
1.7	33.33	23.33	99	90.1	2	2
1.8	75.47	1.07	99	90.1	4	4
1.9	229.39	12.22	99	90.1	4	4
1.10	241.71	41.61	99	90.1	4	4
1.11	325.67	49.61	99	90.1	4	4
1.12	334.34	34.74	99	90.1	4	4
1.13	325.37	49.41	99	90.1	4	4
1.14	99.79	12.21	99	90.1	4	4
1.15	73.41	21.05	99	90.1	4	4
1.16	241.35	12.21	99	90.1	4	4
1.17	225.31	21.32	99	90.1	4	4
1.18	94.34	11.07	99	90.1	4	4
1.19	225.21	19.31	99	90.1	4	4
1.20	33.31	14.24	99	90.1	4	4
1.21	96.57	2.11	99	90.1	4	4
1.22	33.31	12.21	99	90.1	4	4
1.23	25.72	1.01	99	90.1	4	4
1.24	99.79	2.11	99	90.1	4	4
1.25	112.34	17.21	99	90.1	4	4
1.26	27.71	1.01	99	90.1	4	4
1.27	43.34	2.01	99	90.1	4	4
1.28	112.31	24.31	99	90.1	4	4
1.29	75.94	22.04	99	90.1	4	4
1.30	102.71	12.71	99	90.1	4	4
1.31	115.1	14.41	99	90.1	4	4
1.32	102.71	25.71	99	90.1	4	4
1.33	75.94	24.74	99	90.1	4	4
1.34	99.49	18.12	99	90.1	4	4

## FOUNDATION OPTIMIZATION

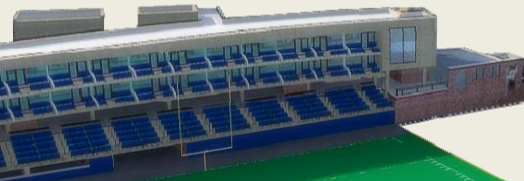
Original Base Shear		New Design Base Shear			
Seismic (Kips)	Wind (Kips)	Seismic (Kips)		Wind (Kips)	
		(Kips)	% Orig.	(Kips)	% Orig.
72	99	62	86%	95	96%
129	162	106	82%	158	98%
102	81	67	66%	77	95%

Wall	Critical Comp. Load (K/Pile)	Critical Tensile Load (K/Pile)	Critical Shear Load (K/Pile)	P<P Allowable	V<V Allowable	Uplift	Original # of Piles	Final # of Piles
SW 1, SW 3, SW 5, & SW7							22	0
SW 2	77	-29	9	OK	OK	YES	10	10
SW 4	142	-27	12	OK	Fail*	YES	10	10
SW 6	61	-21	8	OK	OK	YES	12	12

Supporting	Original # of Piles	Final # of Piles	Difference
Columns	113	110	-3
Shear Walls	54	32	-22
Façade	16	16	0
<b>Total</b>	<b>183</b>	<b>158</b>	<b>-25</b>

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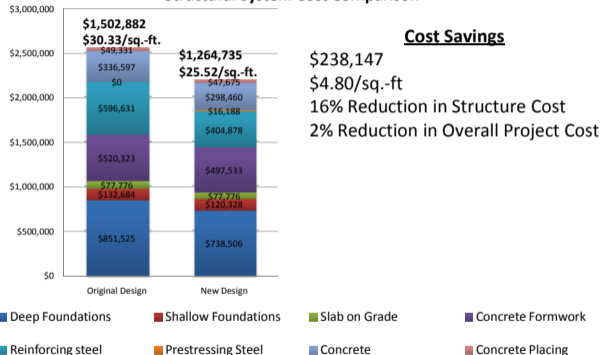
•COST & SCHEDULE ANALYSIS

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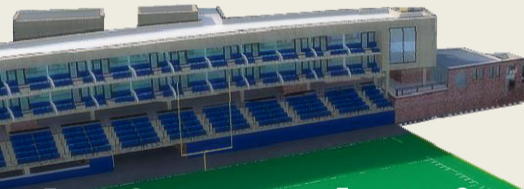
## COST ANALYSIS

Structural System Cost Comparison



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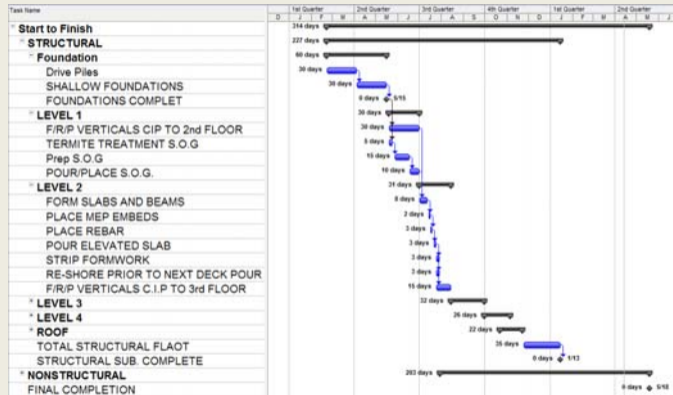
•GRAVITY SYSTEM REDESIGN

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## ORIGINAL DESIGN SCHEDULE



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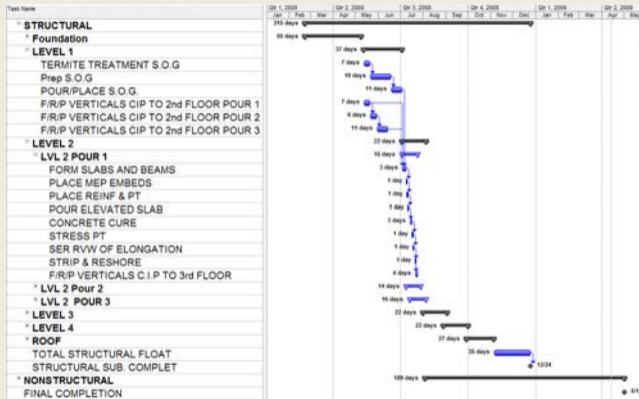
•GRAVITY SYSTEM REDESIGN

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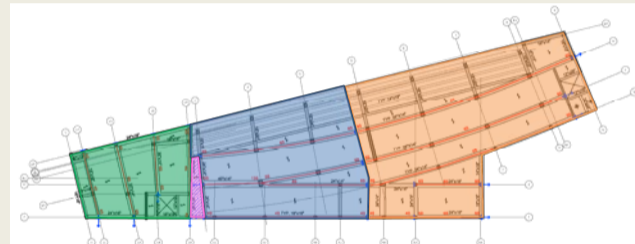
•LATERAL SYSTEM REDESIGN

•CONCLUSIONS

## NEW DESIGN SCHEDULE



## CONSTRUCTION SEQUENCE



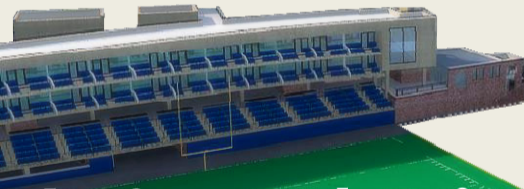
Sequence 2

Sequence 1

Sequence 3

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## LIGHTING REDESIGN





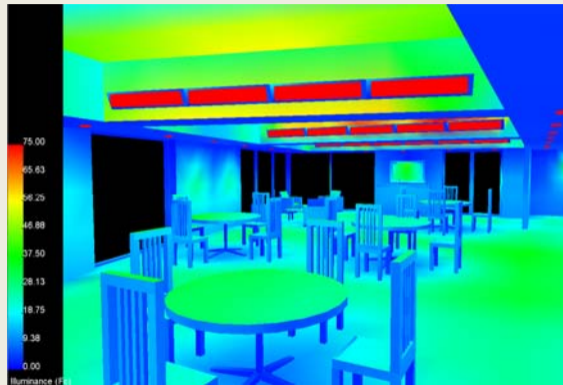
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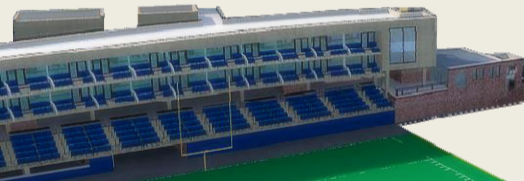
## PSEUDO COLOR RENDERING



# GAME DAY BUILDING

## POST TENSIONED REDESIGN

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## CONCLUSIONS

### Gravity System Redesign

- ✓ Slab depth reduced by 5"
- ✓ Floor depth increase at beams only 2"
- ✓ Buildings weight reduced by 36%

### Lateral System Redesign

- ✓ 4 out of 7 shear walls removed
- ✓ Lateral loading does not control beam design

### Foundation Optimization

- ✓ Number of Piles Reduced by 15%

### Cost and Schedule Analysis

- ✓ \$238,000 in savings
- ✓ Structural erection expedited

### Lighting Redesign

- ✓ Non uniform floor depth can improve aesthetics

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## ACKNOWLEDGEMENTS

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- John Wilson                      Clark Nexsen

### AE Dept. Faculty

- Dr. Walter Schneider III
- Dr. Andres Lepage
- Dr. Linda Hanagan
- Dr. Ali Memari
- Dr. John Messner

### Classmates, Friends, and Family

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QUESTIONS?



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